# **SPIROL**<sup>°</sup> WHITE PAPER

## How to Calculate the Estimated Fatigue Life of a Disc Spring

by John Leckfor, Applications Engineer SPIROL International Corporation, U.S.A.

**Disc Springs** are conically shaped washers designed to provide predictable and repeatable results. This paper focuses on the use of Disc Springs and how to estimate fatigue life in dynamic situations.

In discussing fatigue life, it is important to distinguish between Disc Springs and Conical Spring Washers.

Disc Springs differ from Conical Spring Washers by design and intended usage. Conical Spring Washers are designed to provide a static thrust load in bolted joints and should not be used in fatigue applications. Conical Spring Washers are specified by DIN 6796.

Disc Springs may be used to apply either static or dynamic loads and are specified by DIN EN 16983 (formerly DIN 2093). Typically Disc Springs have a thinner cross section than Conical Spring Washers. Some variation in size is permissible, but calculations only apply to spring steels and when the ratio of the outside diameter to thickness is between 16 and 40 and the ratio of OD to ID between 1.8 and 2.5.

Deflection of a Disc Spring at a given load is predictable making it possible to calculate force and stress levels in the Disc. As the Disc Spring flexes, stress levels in the Disc change; the greater the change, the faster the Disc Spring fatigues.

Tensile stress at points II and III in *Figure 1* are critical in determining fatigue life. These locations are where fatigue cracks originate. Estimation of fatigue life requires evaluation of the maximum stress difference between preload and final load at locations II and III. The location with the highest stress differential is used to estimate fatigue life. Once it is determined which stress values will be used (from location II or III), the fatigue life charts in DIN EN 16983 can be used to estimate the fatigue life of the Disc Spring.



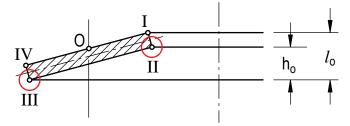


Figure 1: Critical Stress Points within a Disc Spring



Stress values may be found in the Disc Spring product catalog, DIN EN 16983 or calculated using formulas in DIN EN 16984. Fatigue life charts are provided in three thickness ranges: < 1.25mm; between 1.25mm and 6mm and between 6mm and 14mm.

The following examples explain how to interpret the fatigue life charts.

#### Example 1:

Estimate the fatigue life of a DIN EN 16983 Series B Group 2, DSC 50 x 25.4 x 2 Disc Spring with a preload of 15% of its initial height with a final position at 75% of its initial height.

| DIN    | Dimensions                        |      |      |      |      |      |                           | Design Force, Deflection and Stresses Based on<br>E = 206 kN/mm <sup>2</sup> and $\mu$ = 0.3 |                      |                       |     |                         |      |                      |                       |       |                           |                 |        |
|--------|-----------------------------------|------|------|------|------|------|---------------------------|--|----------------------|-----------------------|-----|-------------------------|------|----------------------|-----------------------|-------|---------------------------|-----------------|--------|
| Series |                                   |      |      |      |      |      | Preload, $s = 0.15 h_{o}$ |  |                      |                       |     | s = 0.75 h <sub>o</sub> |      |                      |                       |       | <i>s</i> = h <sub>o</sub> |                 |        |
|        | $D_e$ $D_i$ t $l_o$ $h_o$ $h_o/t$ |      |      |      |      | s    | l <sub>t</sub>            | F  | $\sigma_{_{\rm II}}$ | $\sigma_{_{\rm III}}$ | S   | $l_{\rm t}$             | F    | $\sigma_{_{\rm II}}$ | $\sigma_{_{\rm III}}$ | s     | F                         | σ <sub>om</sub> |        |
| С      | 50.0                              | 25.4 | 1.25 | 2.85 | 1.60 | 1.28 | 0.24                      | 2.61   | 565                  | -11                   | 254 | 1.20                    | 1.65 | 1,550                | 312                   | 1,035 | 1.60                      | 1,646           | -1,006 |
|        | 50.0                              | 25.4 | 1.50 | 3.10 | 1.60 | 1.07 | 0.24                      | 2.86   | 808                  | 32                    | 276 | 1.20                    | 1.90 | 2,512                | 528                   | 1,145 | 1.60                      | 2,844           | -1,207 |
| В      | 50.0                              | 25.4 | 2.00 | 3.40 | 1.40 | 0.70 | 0.21                      | 3.19   | 1,226                | 128                   | 264 | 1.05                    | 2.35 | 4,762                | 923                   | 1,140 | 1.40                      | 5,898           | -1,408 |
|        | 50.0                              | 25.4 | 2.25 | 3.75 | 1.50 | 0.67 | 0.23                      | 3.53   | 1,821                | 165                   | 312 | 1.13                    | 2.63 | 7,217                | 1,147                 | 1,353 | 1.50                      | 8,997           | -1,697 |
|        | 50.0                              | 25.4 | 2.50 | 3.90 | 1.40 | 0.56 | 0.21                      | 3.69   | 2,154                | 204                   | 302 | 1.05                    | 2.85 | 9,063                | 1,301                 | 1,332 | 1.40                      | 11,519          | -1,760 |
| Α      | 50.0                              | 25.4 | 3.00 | 4.10 | 1.10 | 0.37 | 0.17                      | 3.94   | 2,594                | 249                   | 249 | 0.83                    | 3.27 | 11,976               | 1,418                 | 1,135 | 1.10                      | 15,640          | -1,659 |

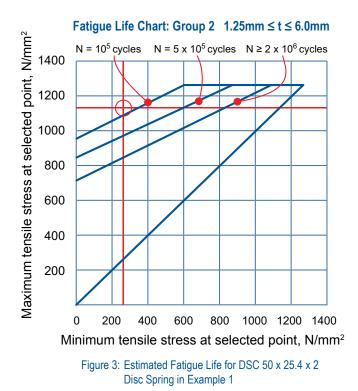
Figure 2: Excerpt from Specification Chart in SPIROL's Disc Spring Catalog

Using the specification chart (shown in *Figure 2*), Stress II ( $\sigma_{\parallel}$ ) at 15% is 128 N/mm<sup>2</sup> and Stress III ( $\sigma_{\parallel}$ ) is 264 N/mm<sup>2</sup>. Stress II ( $\sigma_{\parallel}$ ) at 75% is 923 N/mm<sup>2</sup> and Stress III ( $\sigma_{\parallel}$ ) is 1,140 N/mm<sup>2</sup>. Now calculate the differences between the stress at each location.

|   | <ul> <li>128 N/mm<sup>2</sup></li> <li>Stress II at 15%</li> </ul> | = | 795 N/mm <sup>2</sup> |
|---|--|---|-----------------------|
| , | - 264 N/mm <sup>2</sup><br>Stress III at 15%                       | = | 876 N/mm <sup>2</sup> |

As seen in the calculation above, the maximum differential in stress occurs at location III, therefore we will use the stress values from location III and the fatigue life charts to estimate the fatigue life of the Disc Spring.

The intersection of a vertical line drawn on the X-axis representing the minimum stress at location III and a horizontal line drawn on the Y-axis representing the maximum stress at location III is the estimated fatigue life. In this example and using *Figure 3*, the line on the X-axis is drawn at 264 N/mm<sup>2</sup>, and the line drawn on the Y-axis is drawn at 1,140 N/mm<sup>2</sup>. The intersection is slightly above the "100,000 cycle" line as represented by N = 10<sup>5</sup> in *Figure 3*. This represents an estimated fatigue life of slightly less than 100,000 cycles.

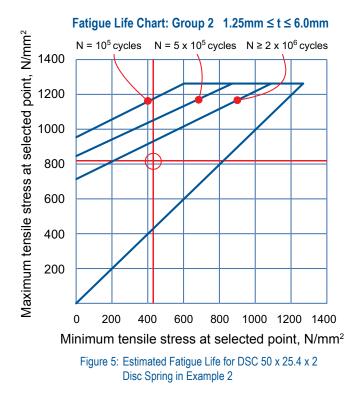


#### Example 2:

Estimate the fatigue life of the same DIN EN 16983 Series B Group 2, DSC 50 x 25.4 x 2 Disc Spring with a preload of 25% of its initial height with a final position at 50% of its initial height:

| <b>DIN</b><br>Series |                | imen | sion | s              |      | Design Force, Deflection and Stresses Based on<br>E = 206 kN/mm <sup>2</sup> and $\mu$ = 0.3 |      |                                |       |                      |                       |      |                               |       |                      |                       |      |                           |                 |
|----------------------|----------------|------|------|----------------|------|--|------|--------------------------------|-------|----------------------|-----------------------|------|-------------------------------|-------|----------------------|-----------------------|------|---------------------------|-----------------|
|                      |                |      |      |                |      |  |      | <i>s</i> = 0.25 h <sub>o</sub> |       |                      |                       |      | <i>s</i> = 0.5 h <sub>°</sub> |       |                      |                       |      | <i>s</i> = h <sub>o</sub> |                 |
|                      | D <sub>e</sub> | D    | t    | l <sub>o</sub> | h₀   | h <sub>₀</sub> /t  | s    | l <sub>t</sub>                 | F     | $\sigma_{_{\rm II}}$ | $\sigma_{_{\rm III}}$ | s    | l <sub>t</sub>                | F     | $\sigma_{_{\rm II}}$ | $\sigma_{_{\rm III}}$ | s    | F                         | σ <sub>om</sub> |
| С                    | 50.0           | 25.4 | 1.25 | 2.85           | 1.60 | 1.28   | 0.40 | 2.45                           | 854   | 2                    | 410                   | 0.80 | 2.05                          | 1,328 | 106                  | 755                   | 1.60 | 1,646                     | -1,006          |
|                      | 50.0           | 25.4 | 1.50 | 3.10           | 1.60 | 1.07   | 0.40 | 2.70                           | 1,242 | 74                   | 447                   | 0.80 | 2.30                          | 2,028 | 250                  | 828                   | 1.60 | 2,844                     | -1,207          |
| В                    | 50.0           | 25.4 | 2.00 | 3.40           | 1.40 | 0.70   | 0.35 | 3.05                           | 1,949 | 230                  | 430                   | 0.70 | 2.70                          | 3,491 | 537                  | 810                   | 1.40 | 5,898                     | -1,408          |
|                      | 50.0           | 25.4 | 2.25 | 3.75           | 1.50 | 0.67   | 0.38 | 3.38                           | 2,905 | 292                  | 508                   | 0.75 | 3.00                          | 5,249 | 675                  | 959                   | 1.50 | 8,997                     | -1,697          |
|                      | 50.0           | 25.4 | 2.50 | 3.90           | 1.40 | 0.56   | 0.35 | 3.55                           | 3,473 | 355                  | 494                   | 0.70 | 3.20                          | 6,437 | 789                  | 938                   | 1.40 | 11,519                    | -1,760          |
| А                    | 50.0           | 25.4 | 3.00 | 4.10           | 1.10 | 0.37   | 0.28 | 3.83                           | 4,255 | 424                  | 409                   | 0.55 | 3.55                          | 8,214 | 897                  | 787                   | 1.10 | 15,640                    | -1,659          |

Figure 4: Excerpt from Specification Chart in SPIROL's Disc Spring Catalog



The maximum differential in stress occurs again at location III. Referencing the fatigue life chart in Figure 5 and plotting 430 N/mm<sup>2</sup> on the X-axis and 810 N/mm<sup>2</sup> on the Y-axis, the intersection of the lines is slightly below the 2 million cycle line; therefore the estimated fatigue life is over 2 million cycles.

These examples highlight how a reduction in deflection results in an increase in fatigue life.

Life charts are based on laboratory testing performed on single Discs at room temperature. Testing is done at a frequency that does not result in heat buildup. Test Discs are lubricated and tested on polished anvils; actual fatigue life is likely to be different than values estimated in the fatigue life charts. These charts are valid for single Discs and stacks of a maximum of (10) Disc Springs in series. Discs Springs stacked in parallel will have reduced fatigue life due to heat buildup resulting from friction.

#### Summary:

Deflection range of the Disc Spring determines its fatigue life. Increasing final load increases stress in the Disc Spring resulting in lower fatigue life. Increasing preload reduces deflection resulting in increased fatigue life. The guidelines provided in this paper are general in nature. Testing is necessary under actual conditions to verify fatigue estimates.



### **Technical Centres**

Europe SPIROL United Kingdom

17 Princewood Road Corby, Northants NN17 4ET United Kingdom Tel. +44 1536 444800 Fax. +44 1536 203415

SPIROL France Cité de l'Automobile ZAC Croix Blandin 18 Rue Léna Bernstein 51100 Reims, France Tel. +33 3 26 36 31 42 Fax. +33 3 26 09 19 76

**SPIROL Germany** Ottostr. 4 80333 Munich, Germany Tel. +49 89 4 111 905 71 Fax. +49 89 4 111 905 72

**SPIROL Spain** 08940 Cornellà de Llobregat Barcelona, Spain Tel. +34 93 669 31 78 Fax. +34 93 193 25 43

SPIROL Czech Republic Sokola Tůmy 743/16 Ostrava-Mariánské Hory 70900 Czech Republic Tel/Fax. +420 417 537 979

**SPIROL Poland** ul. Solec 38 lok. 10 00-394, Warszawa, Poland Tel. +48 510 039 345

Americas SPIROL International Corporation 30 Rock Avenue

Danielson, Connecticut 06239 U.S.A. Tel. +1 860 774 8571 Fax. +1 860 774 2048

**SPIROL Shim Division** 321 Remington Road Stow, Ohio 44224 U.S.A. Tel. +1 330 920 3655 Fax. +1 330 920 3659

SPIROL Canada 3103 St. Etienne Boulevard Windsor, Ontario N8W 5B1 Canada Tel. +1 519 974 3334 Fax. +1 519 974 6550

SPIROL Mexico Avenida Avante #250 Parque Industrial Avante Apodaca Apodaca, N.L. 66607 Mexico Tel. +52 81 8385 4390 Fax. +52 81 8385 4391

SPIROL Brazil

Rua Mafalda Barnabé Soliane, 134 Comercial Vitória Martini, Distrito Industrial CEP 13347-610, Indaiatuba, SP, Brazil Tel. +55 19 3936 2701 Fax. +55 19 3936 7121

Asia SPIROL Asia Headquarters

Pacific 1st Floor, Building 22, Plot D9, District D No. 122 HeDan Road Wai Gao Qiao Free Trade Zone Shanghai, China 200131 Tel. +86 21 5046 1451 Fax. +86 21 5046 1540

SPIROL Korea

160-5 Seokchon-Dong Songpa-gu, Seoul, 138-844, Korea Tel. +86 21 5046-1451 Fax. +86 21 5046-1540

email: info-uk@spirol.com



SPIROL.co.uk